



Overcoming Inefficiencies of Annular Flow in a Hybrid Gas Lift Well

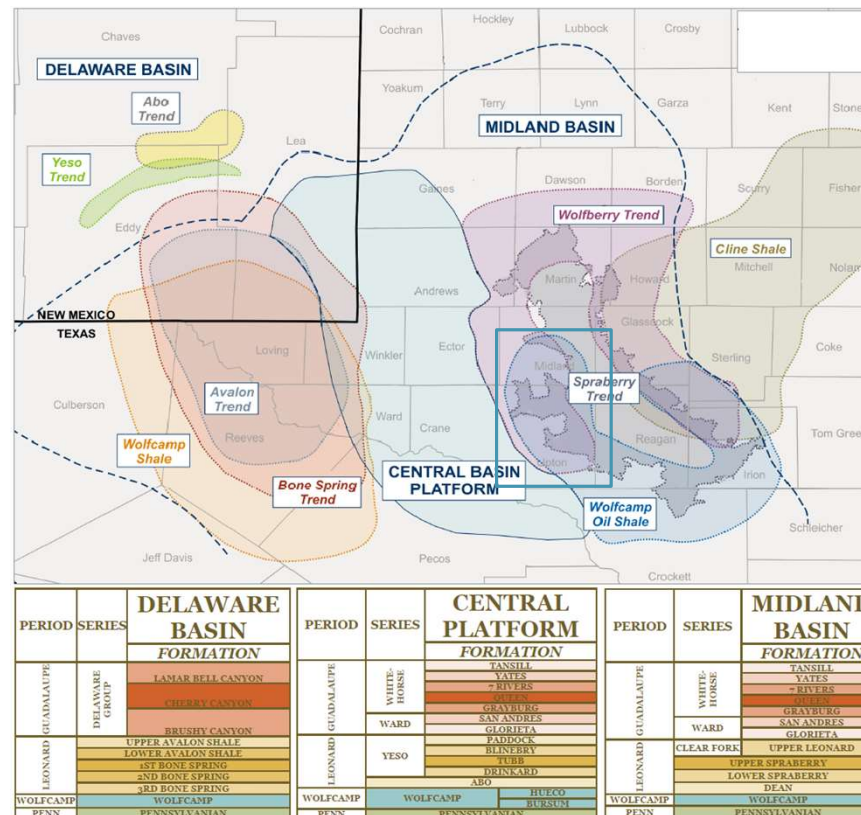
Eric Hale ▶

ALRDC Gas Lift Workshop

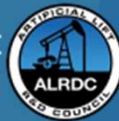
June 7th-11th 2021

Case Study

- ▶ The operator selected the Wolfcamp A formation in the Permian Basin for the case study.
- ▶ Historically this basin has utilized electric submersible pumps (ESP) as the ALS of choice
- ▶ Due to low commodity prices and the multiple re-entries of the wells to repair or downsize the ESP caused the operator to select gas lift as an alternative form for this case study



Artificial Lift Selection



- ▶ Focused on maximizing production rates from the initial production (IP) of the well while maintaining an Artificial Lift System (ALS) designed to minimize work-overs
- ▶ Implemented a dual or “Hybrid” gas lift system to initially produce up the tubing/casing annulus to maximize the IP of the well
 - ▶ Provided a tubing flow option for later life production rates without the need of pulling the original ALS system
 - ▶ Provided an user friendly surface adjustment to meet the goals and needs
 - ▶ Proper selection of gas lift equipment that would allow for later life Plunger Assisted Gas Lift
- ▶ Analysed off-set well production history and Bottomhole Pressures (BHP) data help build a Nodal Analysis data set for ALS review. Analysing the data predicted we could hit forecasted rates with the proper selection of tubing size, landing depth, injection pressure, and volumes.

Slide 3

EH2 Minimizing workovers were key for this project

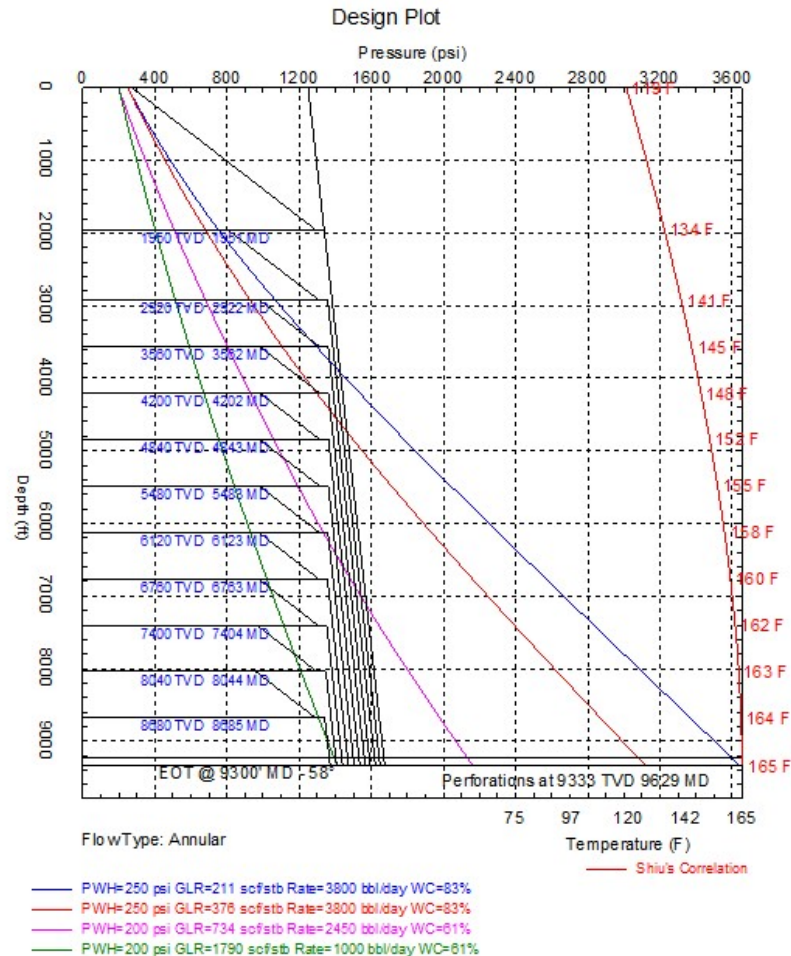
Eric Hale, 5/24/2021

EH3 WIRELINE EQUIPMENT AND SLIDING SLEEVE USED

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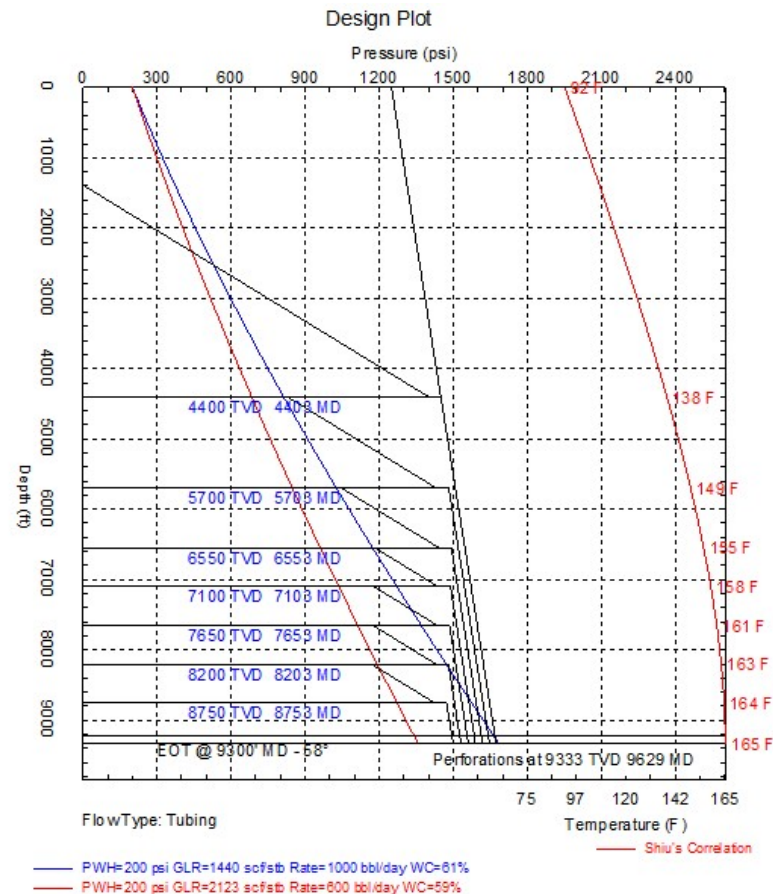
Annular Flow Valve Design Plot-Part #1

- ▶ The 1st part of the Hybrid gas lift system was developed based on the Nodal Analysis review from off-set production and IPR data
- ▶ The system in place accommodated forecasted IP rates as well as the production rates expected when the system would be switched to the 2nd part of the hybrid system



Tubing Flow Valve Design Plot-Part #2

- ▶ The 2nd part of the Hybrid system was developed based on the Nodal Analysis review to help predict liquid loading and unstable flow due to lower/late life production rates flowing up the larger cross-sectional flow area in the tubing/casing annulus.
- ▶ The system in place accommodated late life production rates to ease in the conversion from annular flow to tubing flow



Hybrid Flow Path

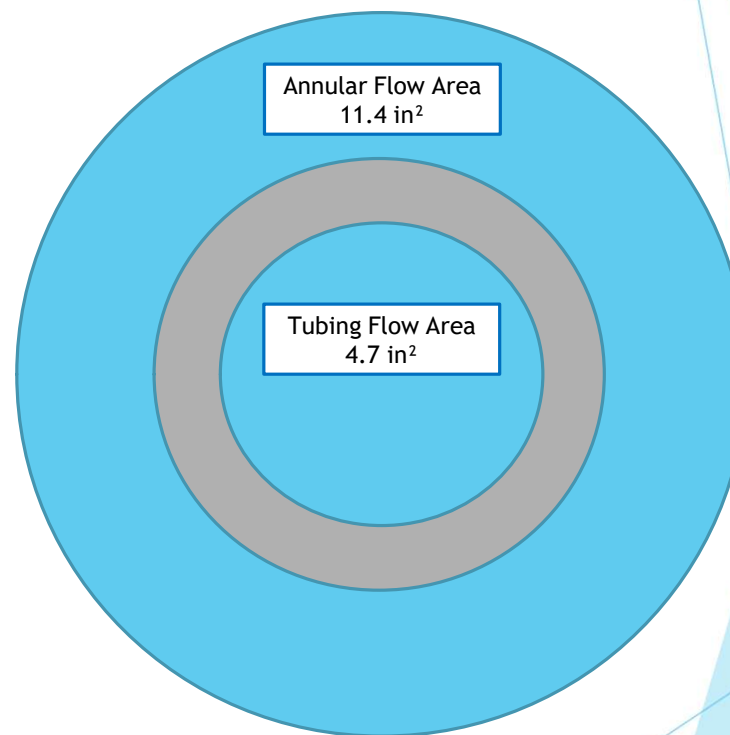
$$\text{Cross Sectional Area} = \pi(C_{id}/2)^2 - \pi(T_{od}/2)^2$$

$$2\text{-}7/8" \quad 6.5\# \quad 2.441" \text{ ID Tubing} = 4.7 \text{ in}^2$$

$$5\text{-}1/2" \quad 20\# \quad 4.778" \text{ ID Casing} = 17.9 \text{ in}^2$$

$$5\text{-}1/2" \times 2\text{-}7/8" \text{ Annular Space} = 11.4 \text{ in}^2$$

$$\text{Equivalent Tubing Flow ID for Annular Space} = 3.816" \text{ ID}$$

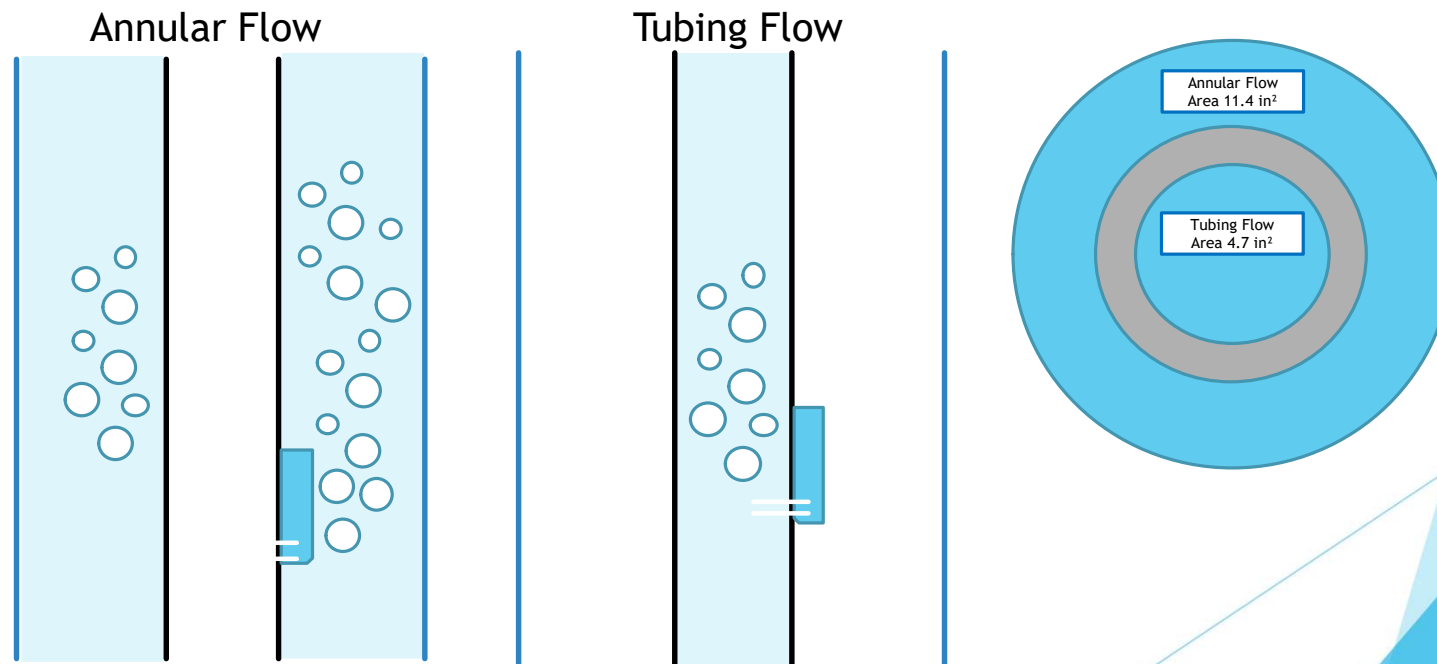


Key Advantages

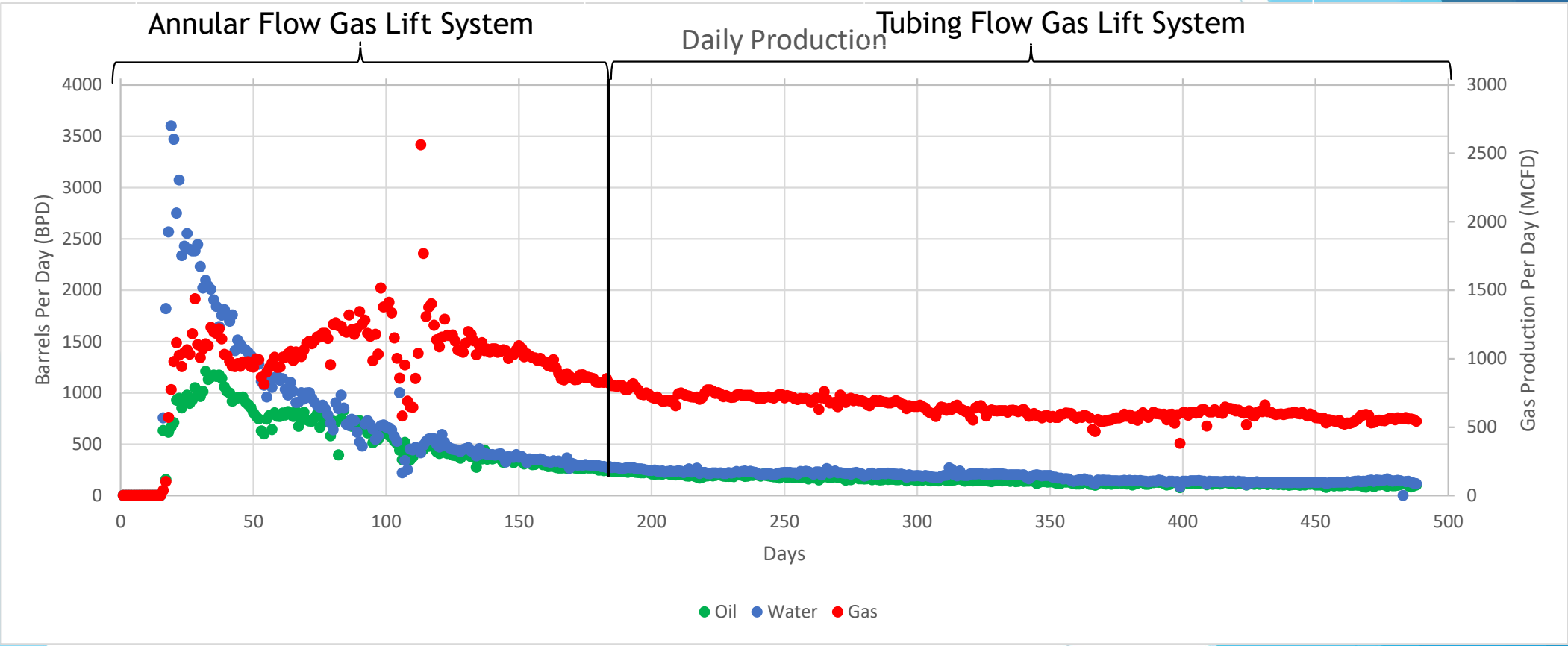
1. Greater flow area compared to conventional tubing flow
2. Reduced flow path friction, lower FBHP

Production Challenges and Goals

- ▶ Utilize the annular portion of the Hybrid System initially to produce the well to full potential and ensure the lowest flowing bottom hole pressure can be achieved
- ▶ Operating the annular flow system from mid-low rates before switching to tubing flow
- ▶ Minimizing the increase in FBHP when switching from annular flow to tubing flow

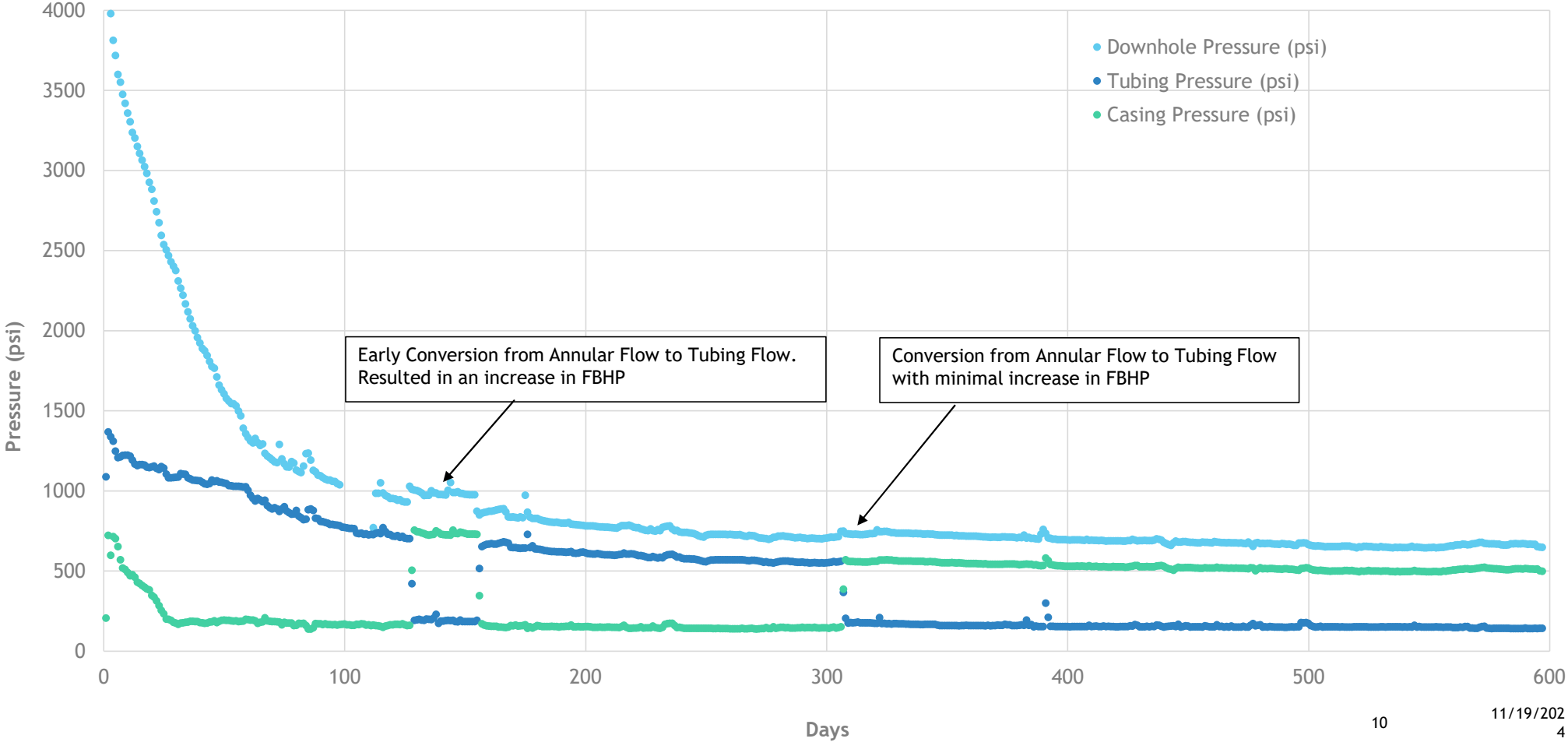


Production History for the Hybrid System



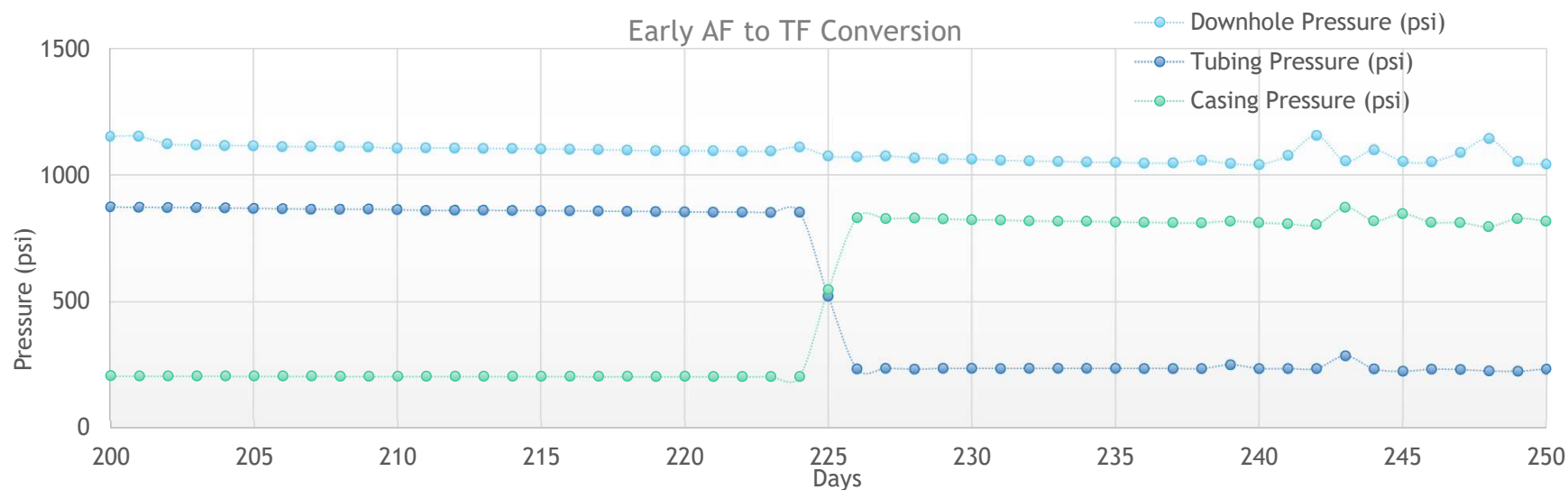
DHG Data

- Downhole Pressure data was closely monitored during the 1st and 2nd part of the Hybrid system to identify the target FBHP when the system should be converted from the Annular Flow to Tubing Flow
- Targeting a minimal change in FBHP was critical to maintaining production while reducing the cross-sectional flow area to help improve flow velocities
- Reduction in injection gas requirements were also key to optimize the system
- The following graphs represent the change in flow area and accommodating FBHP

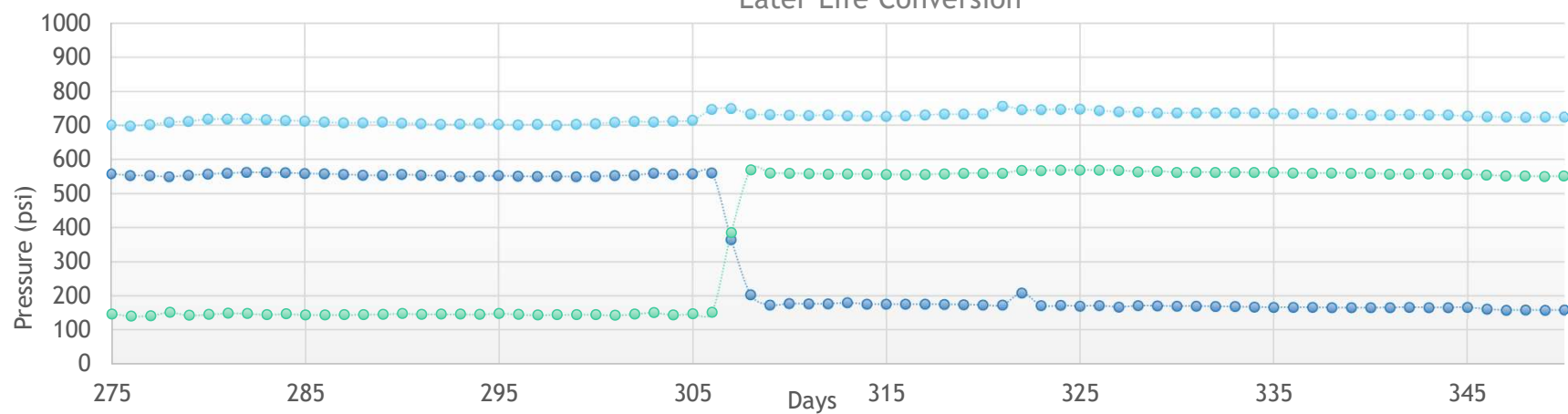




Early AF to TF Conversion

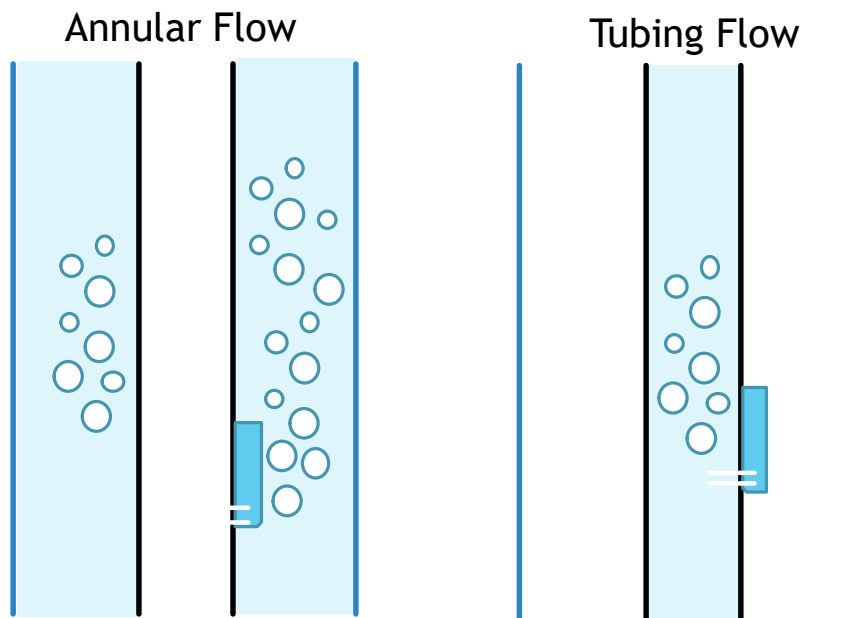


Later Life Conversion



Hybrid Flow Path Conversion

- ▶ The Inflow Performance Relationship (IPR) identifies potential production rates.
- ▶ The IPR helped select tubing size and ideal flow path
- ▶ The IPR identified transition point from annular flow to tubing flow



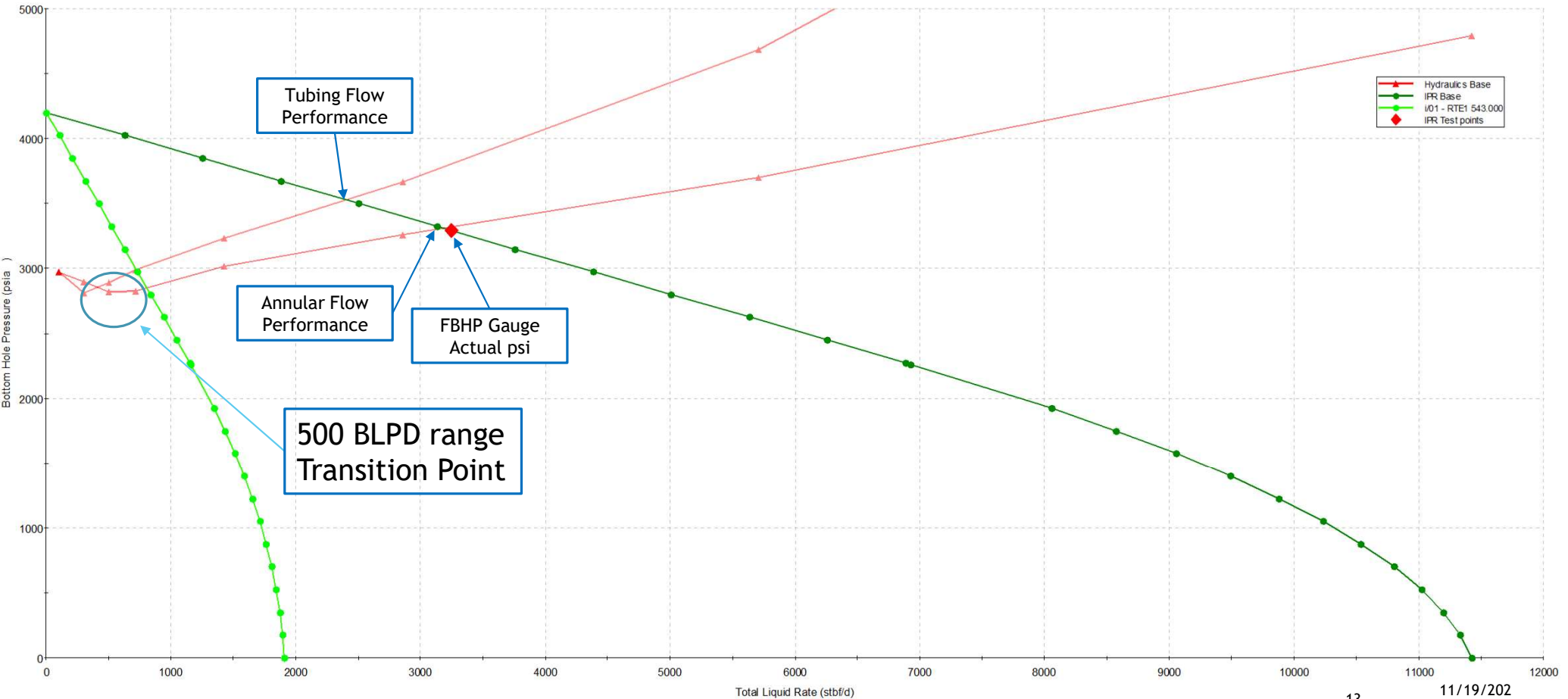
Inflow Performance Relationship (IPR)

Well 23C

Reservoir Data
Pressure = 4200.00 psia

Injected Gas Rate = 258
Lift TV Depth = 2920

WB Depth (MD ft) = 9651
WHPres (psia) = 314.00
Tubing OOD = 2.2873 (s1)



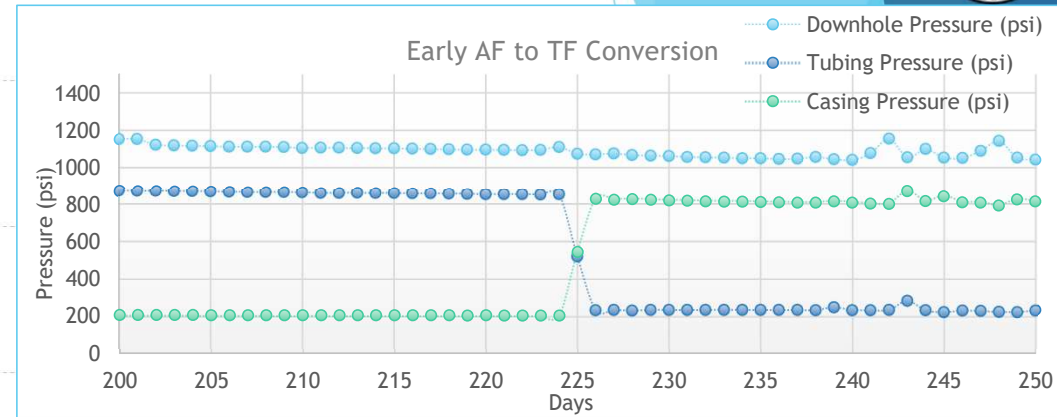
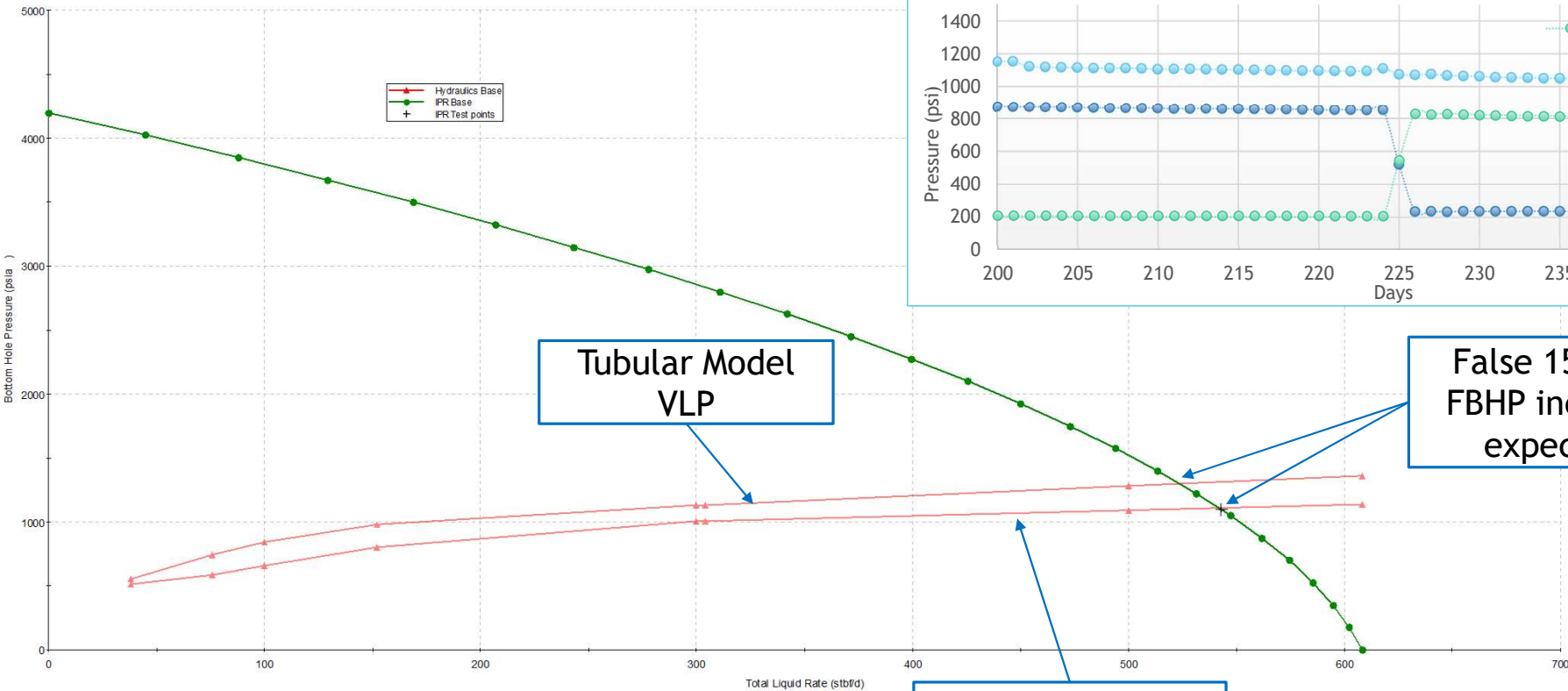
Well 23C Switching Point

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Reservoir Data
Pressure = 4200.00 psia

Injected Gas Rate = 800
Lift TV Depth = 9263



Well 23C Switching Point Velocity Gradient

Reservoir Data
Pressure = 4200.00 psia

Injected Gas Rate = 800
Lift TVDepth = 9263

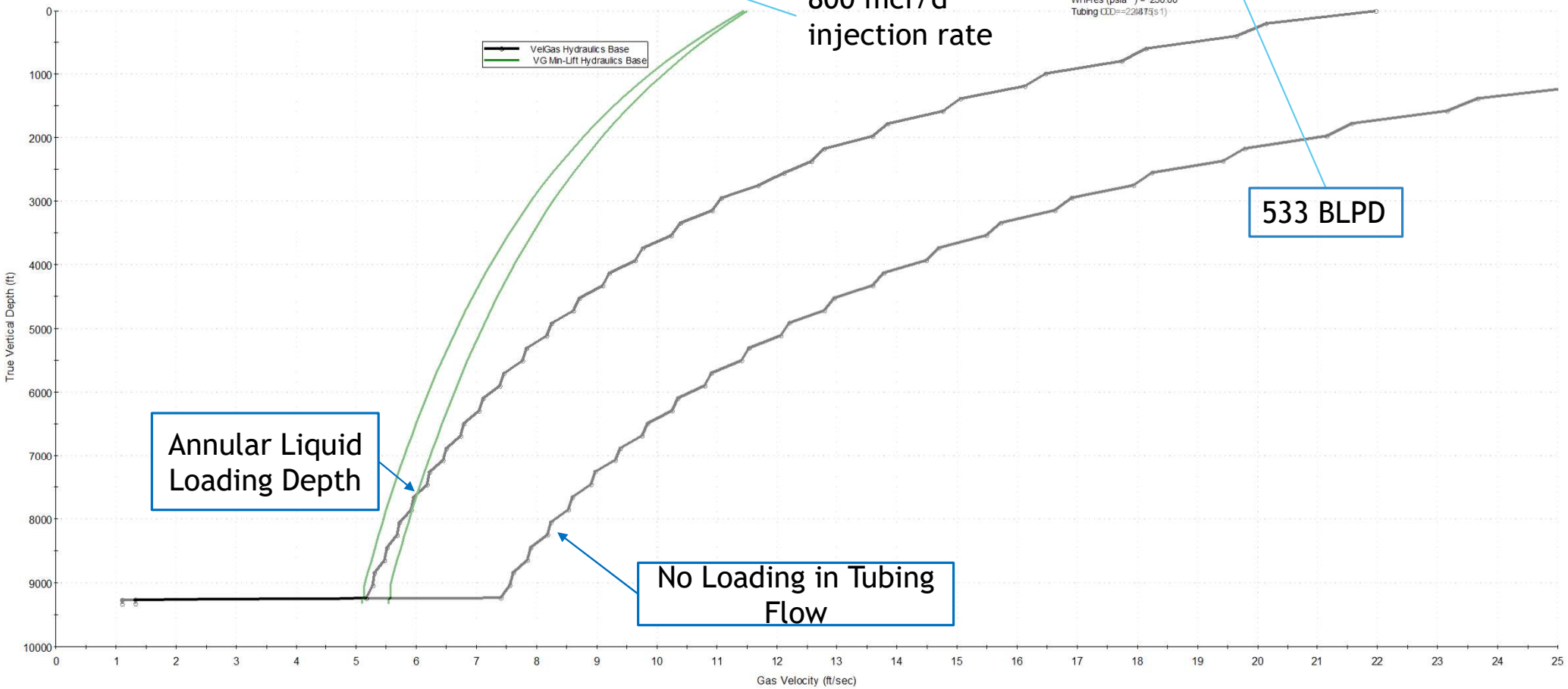
Tubing Gas Velocities 1 @ solution = 532 bpd
22-Jun-20 15:02:36
WB Depth (MD ft) = 9651
WHPres (psia) = 250.00
Tubing ID = 2.2873 (in)

800 mcf/d
injection rate

533 BLPD

Annular Liquid
Loading Depth

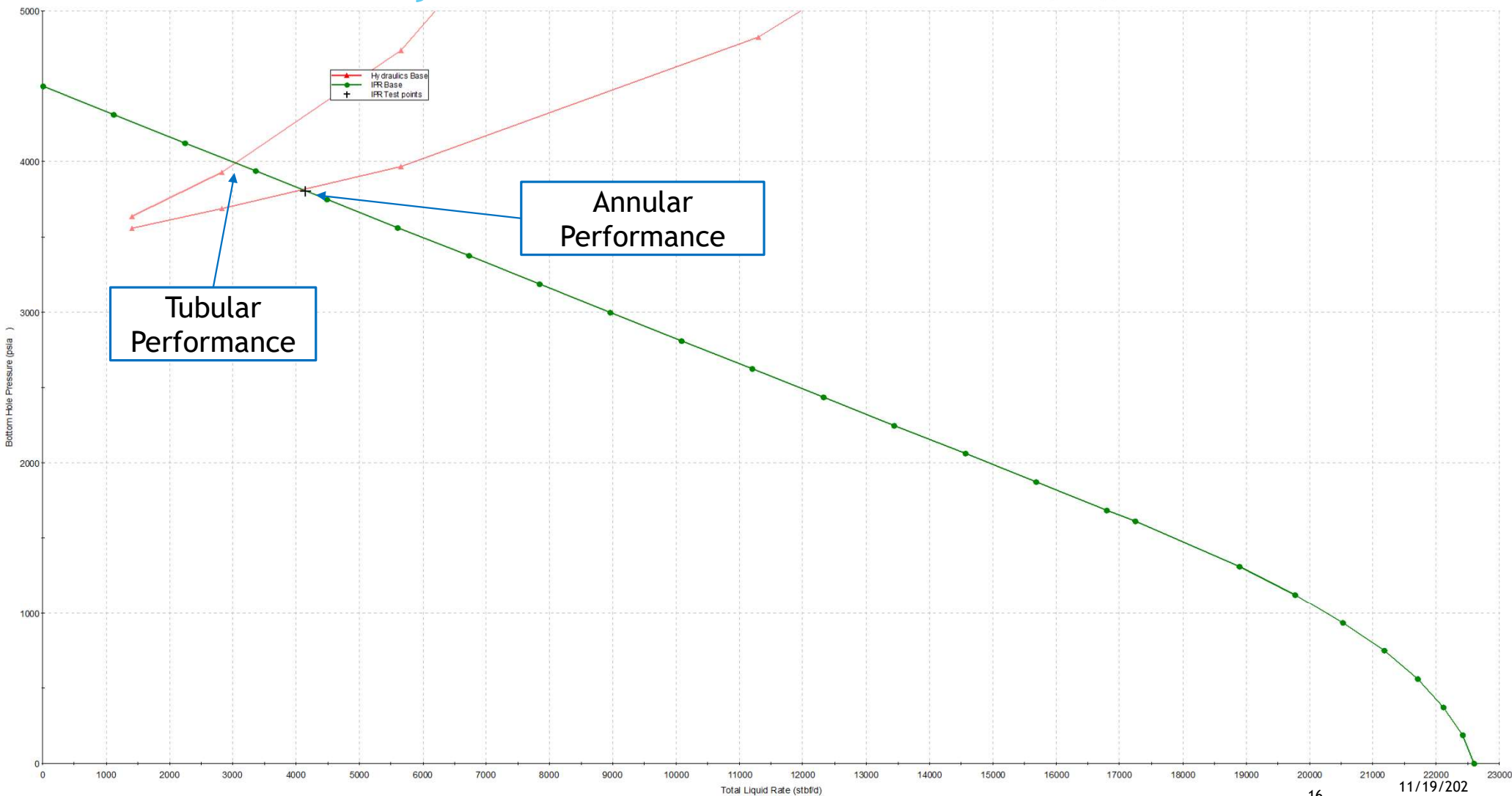
No Loading in Tubing
Flow



Reservoir Data
Pressure = 4500.00 psia

Well 33C Early Life

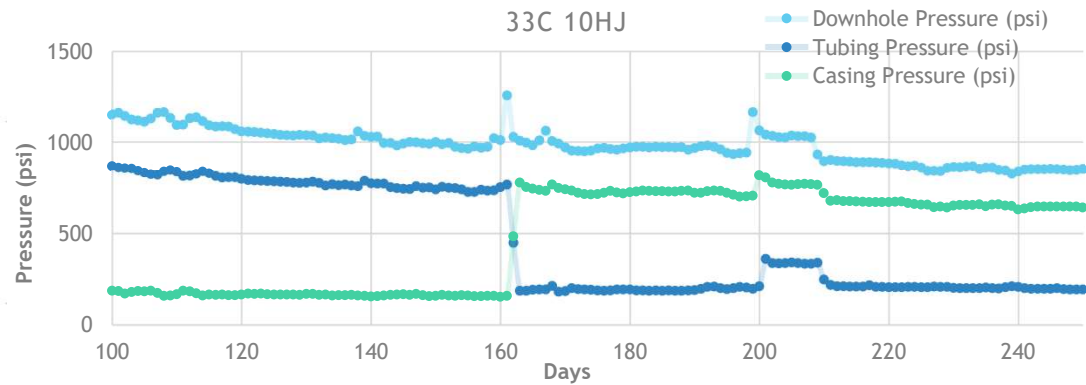
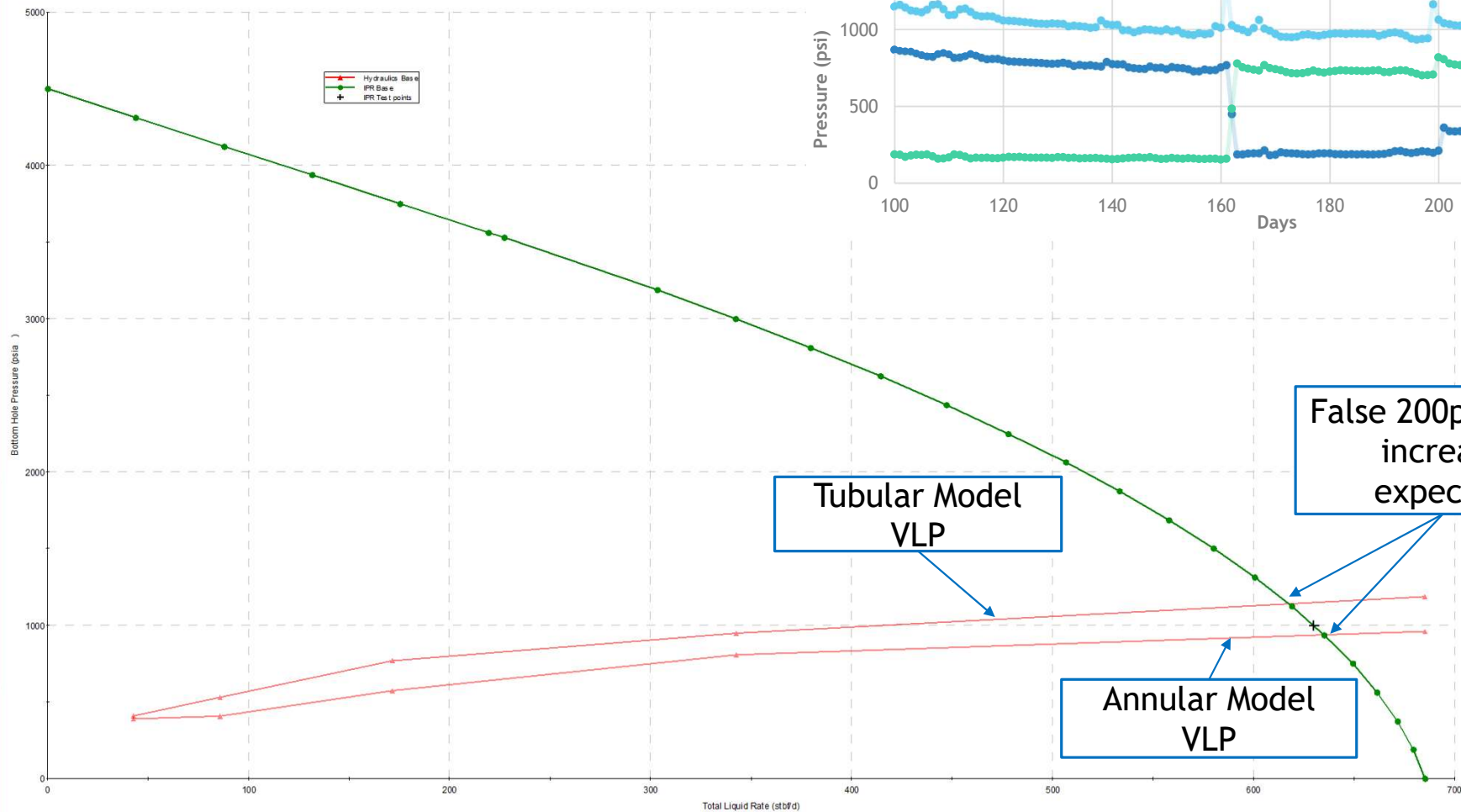
WB Depth (MD ft) = 9625
WHPres (psia) = 400.00
Tubing ID = 2.2475 in



Well 33C Switching Point

Reservoir Data
Pressure = 4500.00 psia

Injected Gas Rate = 1000
Lift TV Depth = 9181



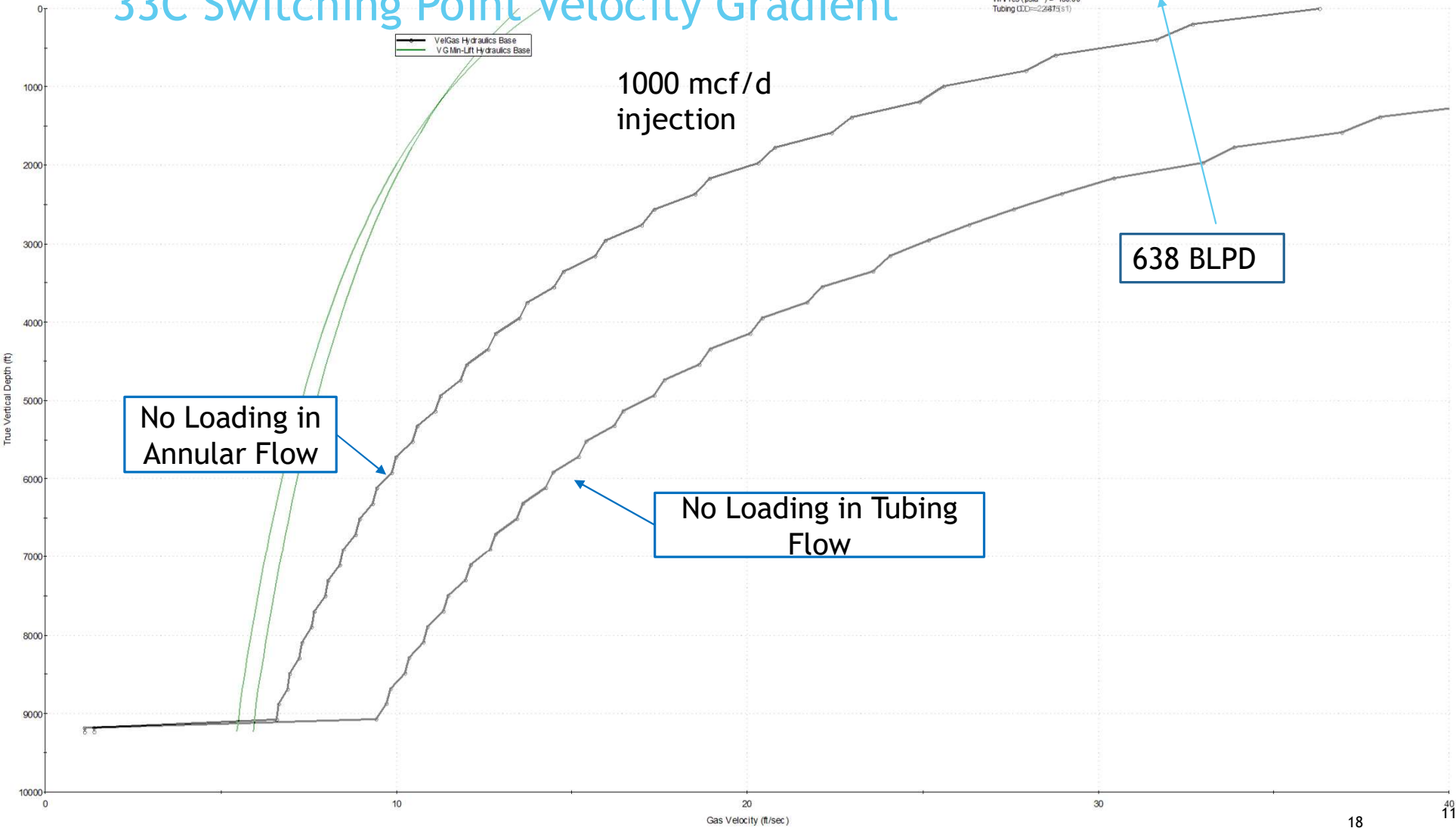
False 200psi FBHP
increase
expected

Reservoir Data
Pressure = 4500.00 psia

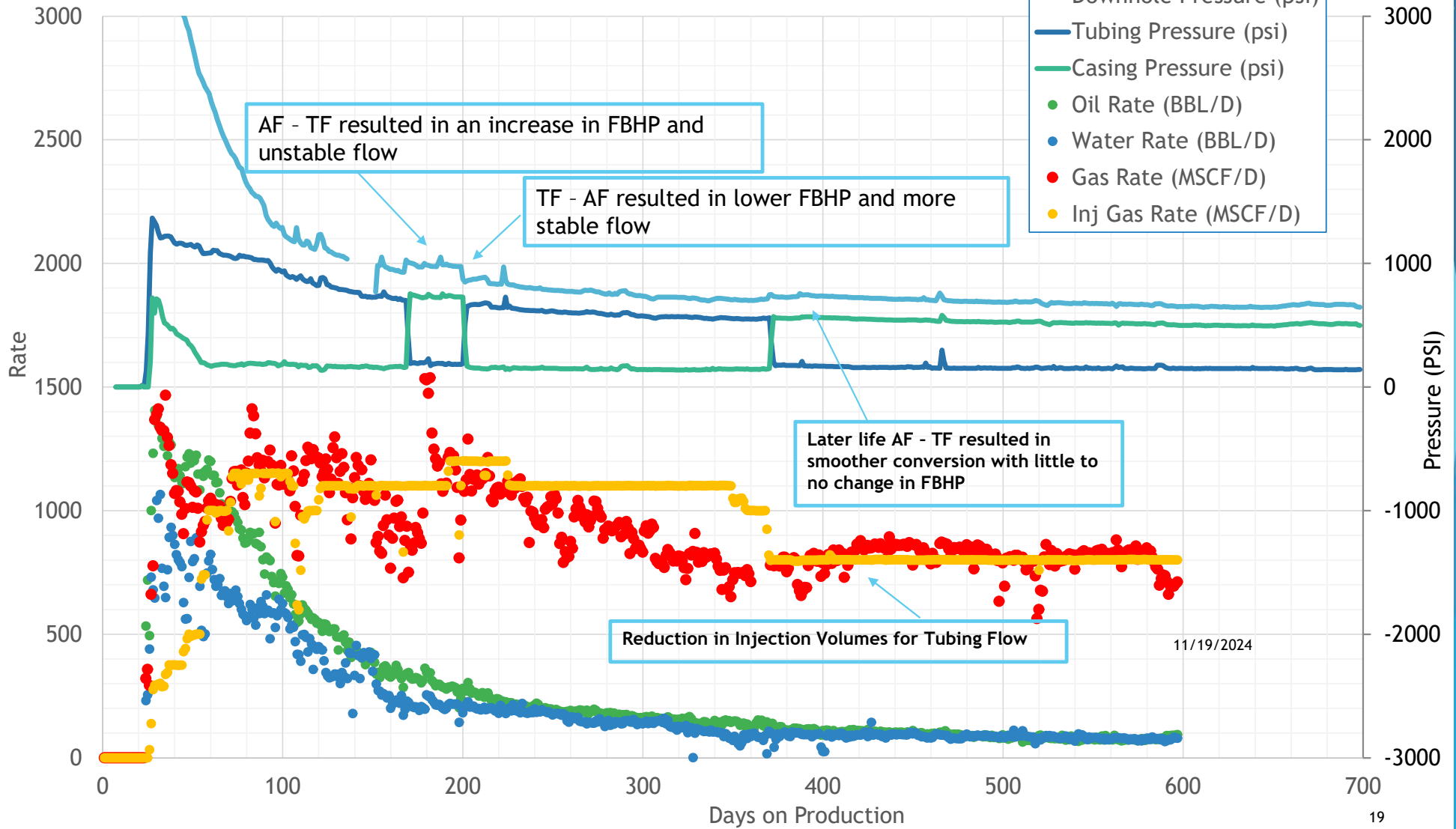
Injected Gas Rate = 1000
Lift TV Depth = 9181

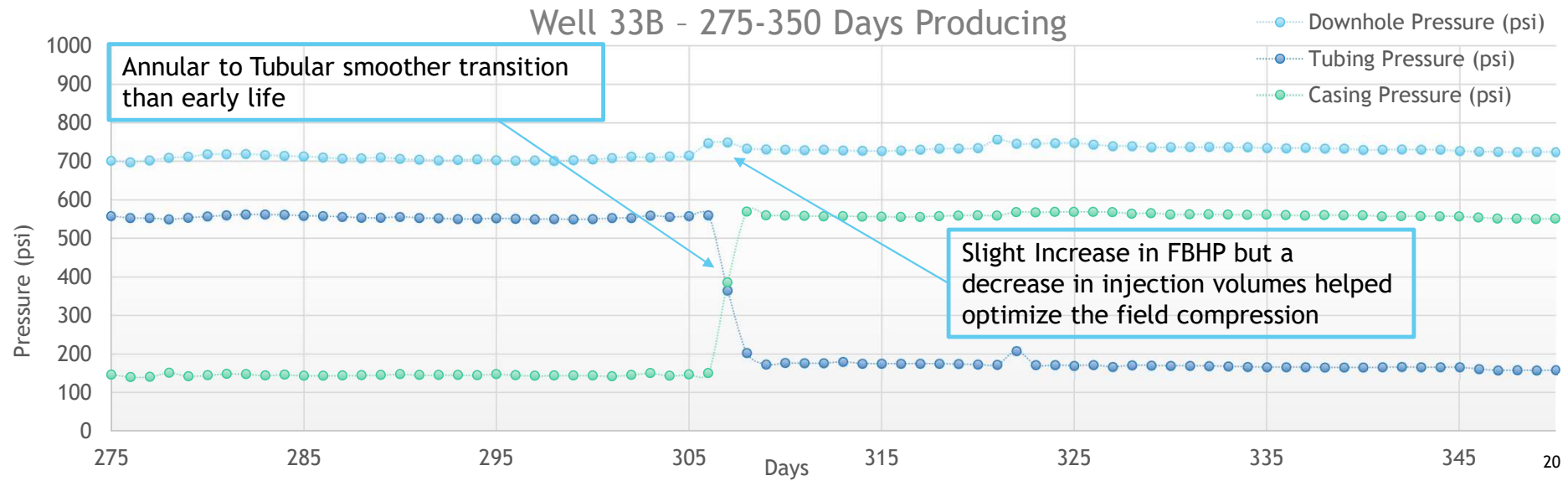
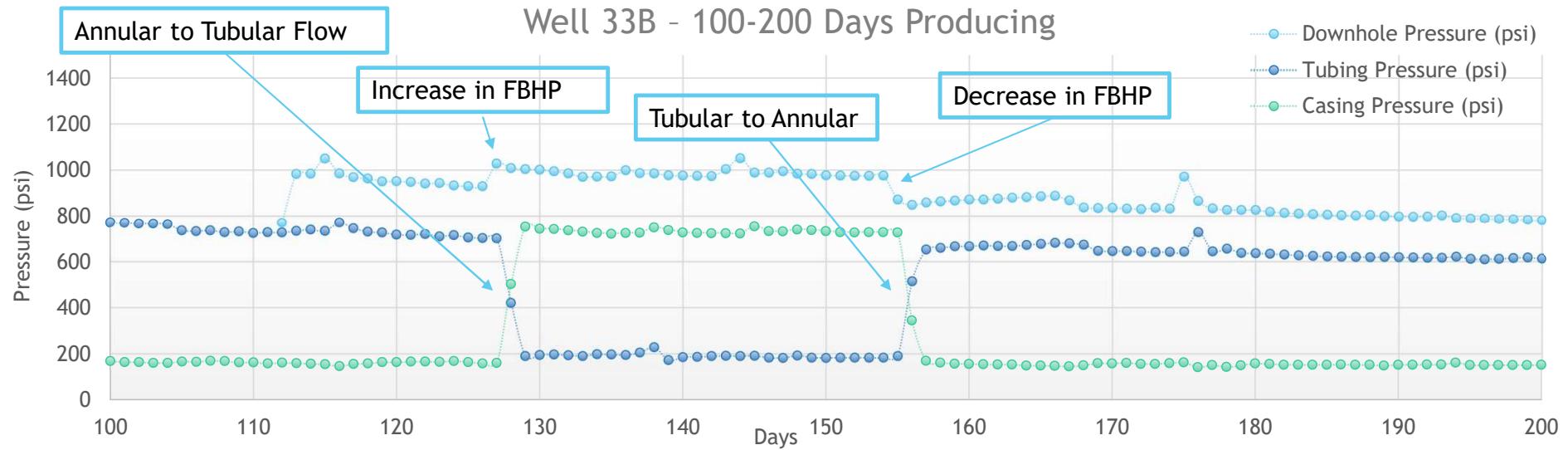
Tubing Gas Velocities 1 @ solution = 633 bpd
24-Jun-20 23:54:23
WB Depth (MD ft) = 9525
WB Pres (psia) = 190.00
Tubing I.D. = 2.4413 (in)

33C Switching Point Velocity Gradient



Well 33B





Lesson Learned

- ▶ Switching from Annular Flow to Tubing Flow too early in the wells production life caused an increase in FBHP and a reduction in production rates as Nodal Analysis predicted
- ▶ Modelling the conversion from annular flow to tubing flow heavily relied upon IPR data and velocity plots to identify and predict liquid loading and unstable flow regimes
- ▶ Adding a secondary wing valve to the B-Section of the wellhead to mitigate erosional concerns
- ▶ Flow off both sides of the casing during Annular Flow to maintain the lowest WHBP



Acknowledgements, & Thank You

Artificial Lift
R&D Council



- ▶ Thank You;

- ▶ *Authors: Charles Kubacak, Lead Production Engineer, Orintiv (Encana Services Co) - Permian South; Matt Young, Sales Director, Flowco Production Solutions*
- ▶ *Nodal Analysis, Graphs, and Visual Aids: Robert Strong, Sales Technical Specialist, Flowco Production Solutions*

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