



**2024 GAS LIFT
WORKSHOP**

Application of Shear Gas Lift Valves in the Pre-Salt Buzios Field

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Goal



To give an overview of the procedure adopted by Petrobras to determine an adequate range of shear-out pressure for the annulus activated gas lift valves in Buzios.

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Agenda

- Motivation: history of failure in gas lift valves
- Gas lift scenario in Buzios
- Design concept of shear gas lift valves
- Technical criteria for determining the shear-out pressure
- Procedure for determining the shear-out pressure in Buzios
- Results
- Final remarks

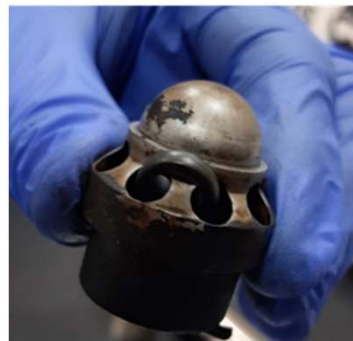


Motivation

- Over 25 cases of **failure in gas lift valves**, since the beginning of pre-salt oil production
- **Symptom:** unwanted flow from tubing to annulus, in the early production stage, before gas lift injection had been initiated in the well
 - High GOR in pre-salt: wells only need artificial lift in specific situations, years after oil production starts
 - Detailed analysis of 6 valves: on average, **663 days** from installation to failure detection

Motivation

- Possible **causes**:
 - Transient effects, opening the check valve
 - Inefficient seal at low pressure differentials
 - Scale deposition (inefficiency of chemical injection system) in some, but not in all, cases
 - Debris



O-ring in undesired position, hindering dart from sealing

Check valve



Nozzle



Venturi



Scale deposition had completely blocked the component



Motivation

- **Consequences:**

- **Well integrity** problem: well barriers were compromised
- At least 14 cases (67% of all cases) have required a rig intervention to replace the damaged valve: significant **cost** increase and production loss
- Cost per intervention \approx 60 gas lift valves

- **Possible solutions:**

- Dummy valves: rig intervention if gas lift injection is needed (additional **cost**)
- **Shear gas lift valves**



Santos Basin, 180 km from the coast of Rio de Janeiro

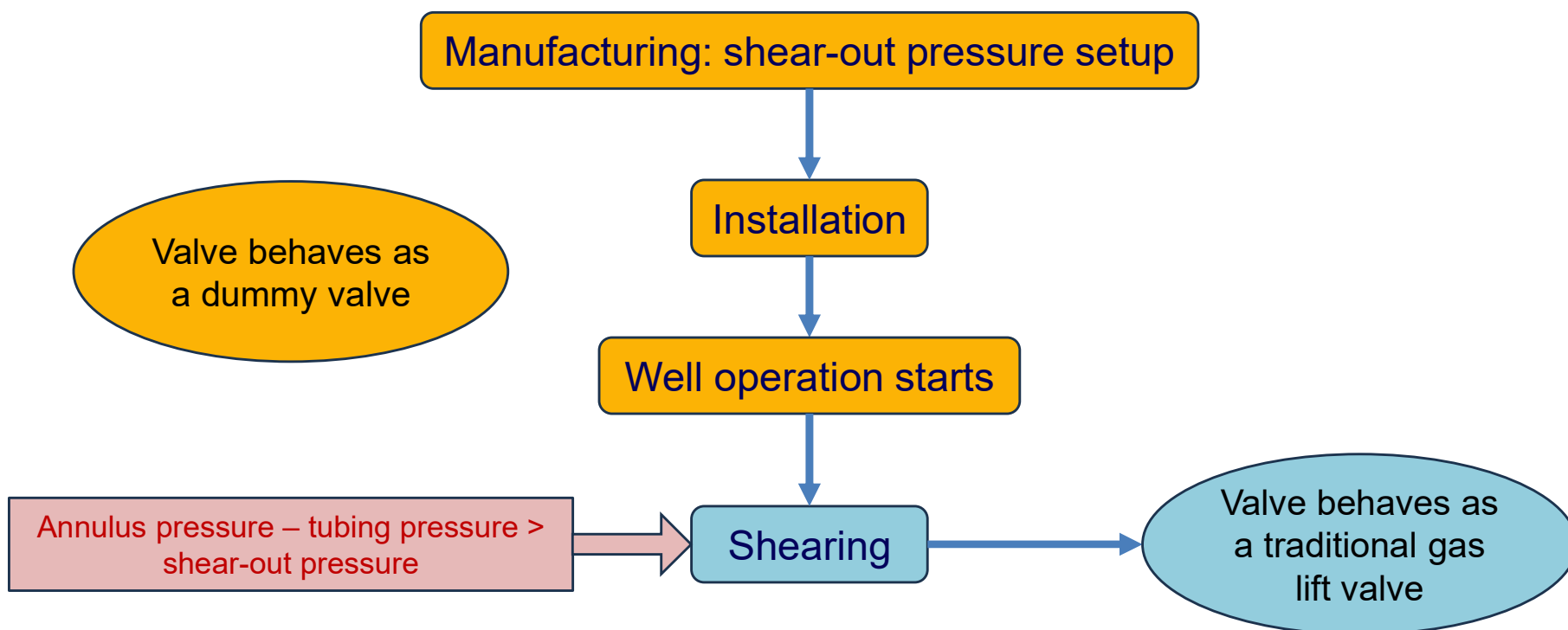
Gas lift scenario in Buzios

- High GOR and WAG injection: wells only **need** artificial lift in specific situations (high water cut combined with low GOR and depletion), which should only occur **5 to 10 years** after oil production starts
- Gas lift is typically **desired** to optimize production (water cut > 60%)
- Occasionally, gas lift is **needed** for stability reasons: intermittence due to geometry, difficulty to restart production after shut-downs
- One Venturi gas lift valve per well
- Intelligent completion in 3 zones, with one chemical injection point per zone



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Design concept of shear gas lift valves



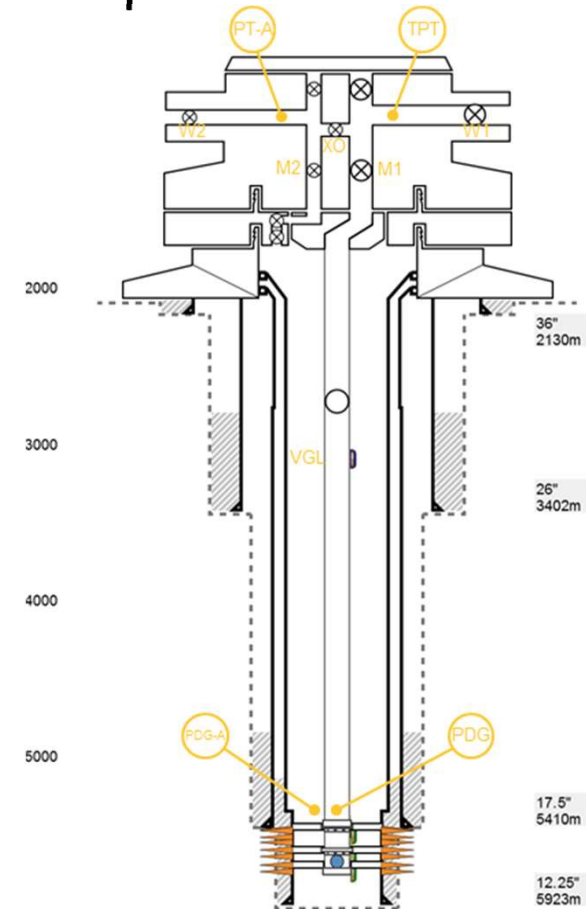


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Technical criteria for determining the shear-out pressure

1) Avoid premature shearing

- Low pressure inside the tubing
- High pressure inside the annulus: heating of confined fluids (Annulus Pressure Buildup – APB), leaks in control lines



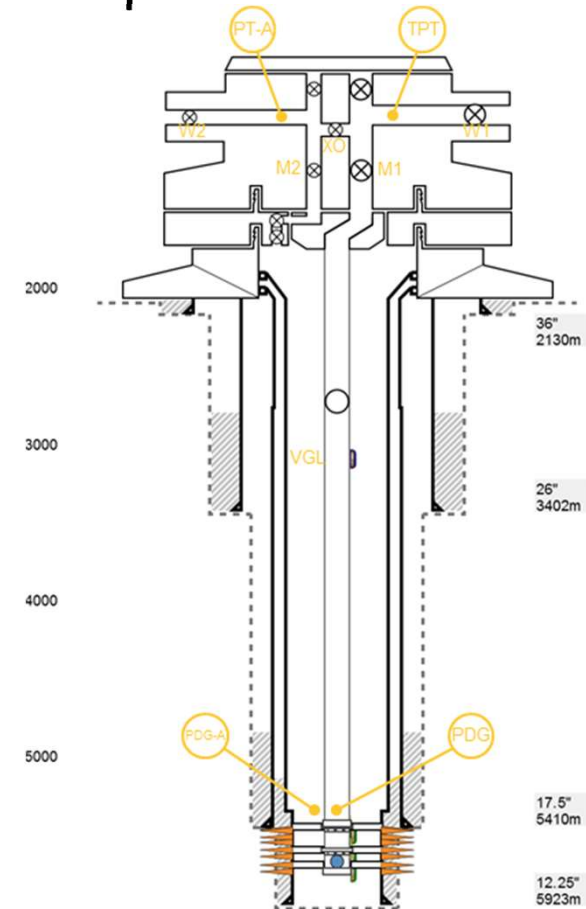
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Technical criteria for determining the shear-out pressure

- 2) Ensure that shearing will occur when needed
 - Shearing during shut-in is desirable
 - Shearing during production must be feasible
 - Maximum available pressure to perform shearing
 - Fluid densities: gas lift/service line, chemical injection line, annulus (completion fluid)
 - Installation depth of the gas lift valve



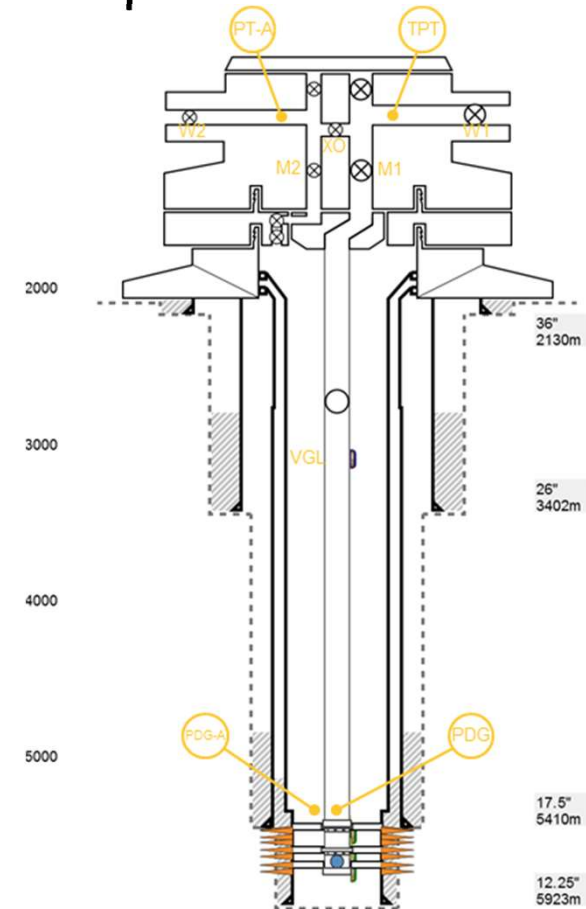
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Technical criteria for determining the shear-out pressure

- 3) Protect the well against structural failure
 - Shearing must occur passively with a smaller differential pressure between annulus and tubing than the failure of completion equipment, even when the expansion of confined fluids due to heating is significant
 - Fuse/circuit breaker: additional layer of protection
- 4) Standardization



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Technical criteria for determining the shear-out pressure

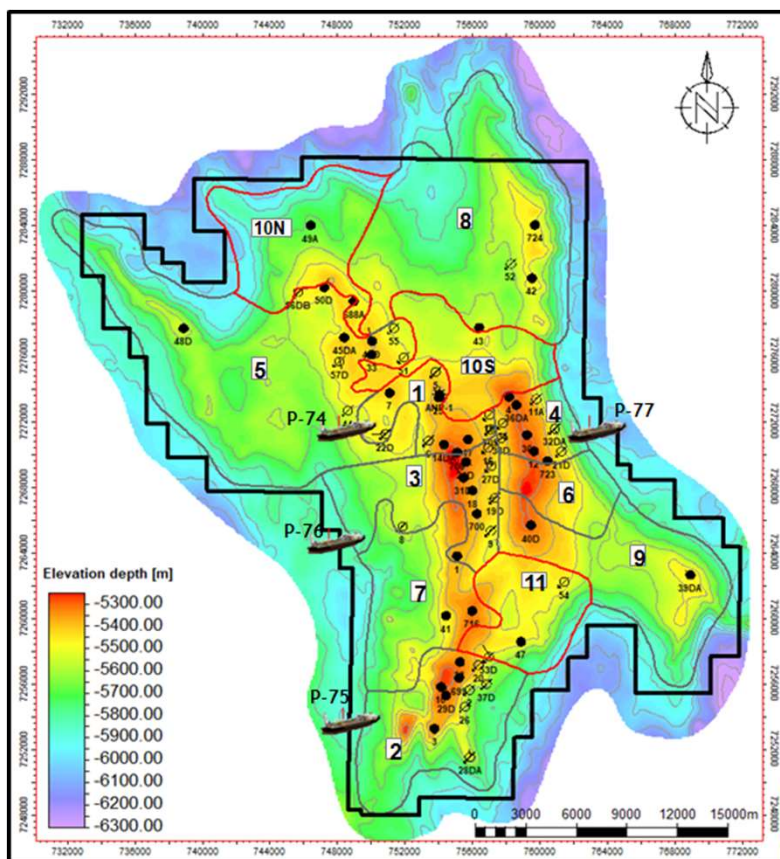
- Safety margins:
 - $\pm 10\%$ admissible error in shear-out pressure set up
 - During well operation, keep $(P_{\text{annulus}} - P_{\text{tubing}}) < 70\%$ of shear-out pressure set up, to avoid premature shearing
 - Shearing must occur when $(P_{\text{annulus}} - P_{\text{tubing}}) = 70\%$ of the differential pressure that results in collapse of the tubing

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Procedure for determining the shear-out pressure in Buzios



Reservoir temperature increases

- Completion of new wells in modules 6-11
- Homogeneous reservoir: high connectivity, same fluid
- At least one representative well per module
- Special cases: data acquisition/exploratory wells
- 5 wells

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Procedure for determining the shear-out pressure in Buzios

- Production curve per well:
 - Maximum and minimum pressures inside the tubing
 - From the moment production starts until gas lift injection starts
 - Pressure and temperature profiles for each selected case (steady-state)



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Procedure for determining the shear-out pressure in Buzios

• Selected cases (for each well):

- First oil
- Maximum and minimum oil flow rate
- Maximum and minimum water flow rate
- Maximum and minimum liquid flow rate
- Maximum restriction at topside
- Maximum and minimum GLR
- Maximum and minimum BHP
- Injection of gas lift starts

Group A

• Selected cases (for the field):

- Maximum oil flow rate
- Maximum water flow rate
- Maximum gas flow rate
- Minimum BHP

Group B

Structural analysis

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Results

- Designing for **Group A** or **Group B** gave us very similar results
- Designing for wells from different production **modules** of the Buzios field gave us very similar results
- The scenario with the highest temperature was the most critical for the structural analysis
- Depending on the well, the range of possible values for the shear-out pressure set up could be as wide as 2500 – 4500 psi
- Standard shear-out pressure set up: $(P_{\text{annulus}} - P_{\text{tubing}}) = \mathbf{3500 \text{ psi}}$

Final remarks

- Safety requirements from the risk assessment analysis:
 - Alleviate pressure from annulus (to gas lift/service line or to production line) when production first starts, to prevent premature shearing
 - Constant monitoring of annulus pressure during well production
- First 3 valves already installed in 2024, with production starting in 2025
- Designing for a well from one of the first production modules of the Buzios field that would suffer a **light workover** intervention gave us a different result:
 - N₂ instead of completion fluid inside the annulus
 - Shear-out pressure set up: $(P_{\text{annulus}} - P_{\text{tubing}}) = \mathbf{3000\ psi}$



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Question Time



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